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### BLEACHABILITY OF KRAFT PULPS TREATED BY ETHANOL-BASED CHLORINE DIOXIDE DELIGNIFICATION SEQUENCES

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**BLEACHABILITY OF KRAFT  
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ETHANOL-BASED CHLORINE  
DIOXIDE DELIGNIFICATION  
SEQUENCES**

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**ABSTRACT**

Kraft pulps delignified with ethanol-based chlorine dioxide ( $D_0$ ) stages yielded pulps with higher brightness levels than aqueous  $D_0$  stages. However, when these pulps were subjected to aqueous extraction (E) stage, the ethanol  $D_0$  pulps were more difficult to brighten with a second chlorine dioxide ( $D_1$ ) stage than were aqueous  $D_0$  pulps. The pulps from a combination of ethanol  $D_0$  and acid ethanol extraction ( $A_E$ ) stages were also more difficult to brighten than aqueous  $D_0E$  pulps. An  $A_E$  stage was less efficient and less selective at removing lignin than an aqueous caustic extraction. Apparently, chromophores are developed in ethanol-based  $D_0$  and  $A_E$  stages that negatively impact  $D_1$  bleachability.

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## INTRODUCTION

Alternatives to conventional kraft pulping and chlorine-based bleaching are being sought to produce strong pulps while minimizing the impact on the environment. Pulping processes that employ ethanol-water solvents would reduce fresh water consumption and possibly eliminate the production of malodorous sulfur compounds during pulping.<sup>2-4</sup> Recently, the application of ethanol-water solutions in ozone bleaching has been evaluated by several investigators<sup>5,6</sup> as a method for increasing ozone bleaching selectivity.

Our studies have examined the use of ethanol-water bleaching media in the first chlorine dioxide delignification ( $D_0$ ) stage<sup>7</sup> and in the first extraction stage.<sup>7-11</sup> Considerable amounts of lignin can be removed from  $D_0$ -treated pulps by an acid ethanol extraction ( $A_E$ ) stage conducted at elevated temperatures (80 to 130°C).<sup>10</sup> An appealing aspect of the  $A_E$  stage is that an ethanol-based partial bleaching sequence could be developed that does not require alternating between acidic and alkaline stages. The effluents from the stages could be combined and evaporated to recover the ethanol and a potentially valuable oxidized lignin for commercial use. Furthermore, the  $D_0$  stage effluent, after pH adjustment, could possibly be used in the  $A_E$  stage, allowing the two to be combined in a ( $D_0/A_E$ ) stage. This would reduce the amount of ethanol needed and increase the economic viability of the  $D_0A_E$  sequence.

In this paper, we examine how the  $A_E$  medium (i.e.,  $D_0$  effluent or fresh ethanol-water solution) influences  $A_E$  stage delignification. Comparisons are made between an optimized  $D_0A_E$  and aqueous  $D_0E$  sequence in terms of delignification, incremental brightness development, and  $D_1$  bleachability. Also, in this report, we examine the impact of the  $D_0$  stage bleaching medium on  $D_1$  bleachability.

## RESULTS AND DISCUSSION

### Initial $D_0A_E$ and ( $D_0/A_E$ ) Bleaching Results

Several small-scale experiments were performed to ascertain the optimum conditions for delignification and selectivity for the ethanol-based  $D_0A_E$  sequence. Most of the initial conditions chosen for the  $A_E$  stage were based on our previous study.<sup>10</sup> Approximately 50% of the residual lignin was removed with the  $D_0A_E$  sequence (Table 1). The bulk of this delignification (~35%) occurred within the  $D_0$  stage. Two interesting observations were made with this sequence. First, the brightness of the pulp



**Table 1.** Initial Results from Ethanol-Based  $D_0A_E$  and  $(D_0/A_E)$  Partial Sequences

	$A_E$ stage reaction time (hrs.)	Kappa number	Residual lignin (%)	ISO brightness (%)
Unbleached	–	30.1	4.63	19.7
$D_0$	–	13.2	3.02	34.5
$D_0A_E$	2.5	9.3	2.18	24.0
$D_0A_E$	5.0	9.4	2.27	26.0
$(D_0/A_E)$	1.0	9.6	2.18	27.1
$(D_0/A_E)$	2.5	7.8	1.78	29.0
$(D_0/A_E)$	5.0	7.2	1.83	27.5

decreased by 8 to 10 points across the  $A_E$  stage, and second, the  $A_E$  stage pH decreased from 4.2 to 3.5. This pH drop was not observed in our earlier study,<sup>10</sup> probably because the consistency used in that study (1.25%) was lower than in the present one (3.0%).

### Effect of $A_E$ Stage pH on Delignification

A second series of experiments employed the  $D_0$  stage effluent as the ethanol-water medium in the  $A_E$  stage (Table 1). Such a bleaching sequence has no interstage washing and was denoted as  $(D_0/A_E)$ . Surprisingly, the  $(D_0/A_E)$  sequence was more efficient at delignification than the  $D_0A_E$ . This enhancement could be caused by the reaction of trace amounts of chlorite  $ClO_2^-$  in the extraction medium. The bulk of the lignin removal with an  $A_E$  stage occurred within the first 2.5 hours of extraction. The pulp brightness and pH decreased during the  $A_E$  stage of the  $(D_0/A_E)$ ; a similar decrease was observed in the  $D_0A_E$  sequence.

Increasing the initial  $A_E$  pH from 4.2 to 5.8 was detrimental for lignin extraction (Table 2). The poorer  $A_E$  delignification, particularly for the  $D_0A_E$  sequence, was likely related to the conversion of the carboxylic acids in the oxidized lignin to their sodium salts. A previous study<sup>9</sup> indicated that oxidized lignin has a lower *alkali* solubility in ethanol-water media than in water. Almost all of the increase in pulp brightness with the  $D_0$  stage was lost when the  $A_E$  stage was operated at the higher pH levels.

Furthermore, with the high-pH  $A_E$  stage of the  $(D_0/A_E)$  sequence, there appeared to be some lignin condensation reactions, as evidenced by the increases in kappa number and residual lignin. Such increases could be related to condensation reactions between dissolved oxidized lignin and the



**Table 2.** Effect of  $A_E$  Exit pH on  $D_0A_E$  and  $(D_0/A_E)$  Bleaching (5-hr.  $A_E$  stage)

EtOH-based sequence	$A_E$ stage pH		Kappa number	Residual lignin (%)	ISO brightness (%)
	Initial	Final			
Unbleached	–	–	30.1	4.63	19.7
$D_0$	–	–	13.2	3.02	34.5
$D_0A_E$	4.2	3.5	9.4	2.27	26.0
$D_0A_E$	5.8	5.1	11.9	2.60	20.0
$(D_0/A_E)$	4.2	3.5	7.2	1.83	27.5
$(D_0/A_E)$	5.8	4.8	15.3	3.20	16.8

**Table 3.** Effects of pH and  $\text{ClO}_2^-$  in the  $A_E$  on  $D_0A_E$  and  $(D_0/A_E)$  Bleaching (2.5-hr.  $A_E$  stage)

EtOH-based sequence	$A_E$ stage end pH	Kappa number	Residual lignin (%)	ISO brightness (%)
Unbleached	–	30.1	4.63	19.7
$(D_0/A_E)$	4.1	9.3	2.12	34.5
$(D_0/A_E)$	3.9	8.3	2.00	25.4
$(D_0/A_E)$	3.6	8.1	1.91	26.3
$(D_0/A_E)$	3.4	7.8	1.78	29.0
$D_0A_E$ (w/ 0.2mM of $\text{ClO}_2^-$ in $A_E$ )	3.5	7.8	1.75	28.7
$D_0A_E$	3.6	9.3	2.18	24.0

lignin in the fiber; Simson *et al.*<sup>12</sup> and Brage *et al.*<sup>13</sup> report that quinonoid structures can condense with themselves under mildly acidic reaction conditions.

Additional small-scale trials evaluated minor changes in the  $A_E$  stage pH on  $(D_0/A_E)$  bleaching (Table 3). Adjusting the final  $A_E$  stage pH from 3.5 to 4.1 gradually decreased the overall amount of residual lignin removed and the brightness level obtained with the  $(D_0/A_E)$  sequence. The increased delignification efficiency of the  $(D_0/A_E)$  sequence with lower  $A_E$  stage pH is presumably related to trace amounts of  $\text{ClO}_2^-$  in the  $A_E$  medium. Several studies have noted the increased reactivity of  $\text{ClO}_2^-$  with various lignin model compounds as the pH of the medium is decreased from 4 to 3.<sup>13–16</sup>

An  $A_E$  stage was conducted with fresh ethanol that contained 0.20 mM of  $\text{ClO}_2^-$  (Table 3). This experiment was performed to ascertain if trace levels of  $\text{ClO}_2^-$  in the  $A_E$  medium improves delignification. The addition of  $\text{ClO}_2^-$



enhanced both lignin removal and brightness development of the  $D_0A_E$  sequence to comparable levels of the  $(D_0/A_E)$  sequence. Thus, it appears that the improved performance of the  $(D_0/A_E)$  sequence is related to trace levels of  $ClO_2^-$  in the  $A_E$  medium. We have found 0.2–0.3 mM  $ClO_2^-$  in ethanol-based  $D_0$  stage effluents.<sup>7</sup>

### Effect of $(D_0/A_E)$ on Pulp Viscosity and Zero-Span Strength

The results of the previous section indicated that the optimum  $A_E$  exit pH for  $(D_0/A_E)$  delignification is  $\sim 3.5$ . However, acid hydrolysis of the glycosidic bonds in cellulose can become significant at pH levels below 4 when elevated temperatures are used ( $> 100^\circ C$ ).<sup>7,10</sup> Indeed, the  $A_E$  stage significantly contributed to carbohydrate degradation and pulp strength loss as noted by pulp viscosity and zero-span breaking length strength measurements (Table 4). The amount of pulp damage at the higher exit pH (3.9) was unexpected, based on our earlier observations.<sup>10</sup> One expects a 1 to 4 mPa·s decrease in pulp viscosity across an aqueous  $D_0E$  or  $D_0(EO)$  sequence.<sup>7,17,18</sup> The  $(D_0/A_E)$  sequence was much more aggressive at carbohydrate degradation ( $\sim 7$  to 9 mPa·s decrease).

### Bleachability of $(D_0/A_E)$ Versus Aqueous-Based $D_0E$ Delignified Pulps

Large-scale runs of the ethanol-based  $(D_0/A_E)$  sequence were performed to produce enough pulp to conduct a  $D_1$  bleachability trial (Table 5). These larger scale runs yielded pulps with higher kappa numbers, higher residual lignin values, and lower brightness levels than the corresponding

**Table 4.** Effect of Exit pH on  $(D_0/A_E)$  Carbohydrate Degradation (2.5-hr  $A_E$  stage)

	$A_E$ stage exit pH	Viscosity (mPa·s)	Zero-span breaking length	
			Wet (km)	Dry (km)
Brownstock	–	25.1	16.0	20.8
$D_0$	–	24.5	16.2	21.0
$(D_0/A_E)$	3.5	16.4	6.7	12.7
$(D_0/A_E)$	3.9	18.6	10.0	16.2



**Table 5.** Comparison of the Ethanol-Based ( $D_0/A_E$ ) and Aqueous  $D_0E$  Sequences

Bleaching sequence <sup>†</sup>	$A_E$ stage exit pH	Kappa number	Residual lignin (%)	ISO brightness (%)	$k_{457}$ ( $m^2/kg$ )
Aqueous $D_0$	–	16.6	2.98	32.9	4.8
Ethanol-based $D_0$	–	13.3	2.99	34.7	3.8
Aqueous $D_0E$	–	7.3	1.37	38.5	3.6
( $D_0/A_E$ )	3.6	9.8	2.37	22.9	11.8
( $D_0/A_E$ )	3.9	11.9	2.64	21.7	13.9
( $D_0/A_E$ )E	3.6	8.7	1.51	29.2	7.9
( $D_0/A_E$ )E	3.9	9.0	1.73	27.6	8.3

<sup>†</sup>All E stages performed with 100% aqueous medium; 2.5-hr.  $A_E$  stage.

small-scale ( $D_0/A_E$ ) runs. The reason this occurred is unclear. The results from these large-scale ( $D_0/A_E$ ) stages are almost comparable to the small-scale  $D_0A_E$ , possibly indicating that there was no residual  $ClO_2^-$  in the  $A_E$  medium.

The aqueous-based  $D_0E$  sequence was more efficient at lignin removal and brightness development than the ( $D_0/A_E$ ) sequence. Nevertheless, an ethanol-based  $D_0$  yielded a brighter pulp than its aqueous counterpart; this result agrees with our earlier observations<sup>7</sup> and will be discussed later in this report. Additional residual lignin was removed from the ( $D_0/A_E$ )-treated pulp using an aqueous E stage (Table 5, entries 6 and 7). However, the E stage treatment did not increase the brightness or decrease the light absorption coefficient ( $k_{457}$ ) to the post- $D_0$  values (34.7 ISO and 3.8  $m^2/kg$ , respectively).

Some preliminary aqueous  $D_1$  bleaching trials were conducted on the  $D_0E$ , ( $D_0/A_E$ ), and ( $D_0/A_E$ )E pulps (Table 6). The  $D_1$  stages performed directly on a ( $D_0/A_E$ ) pulp yielded a modest 23-point increase in brightness; an aqueous E-stage treatment of a ( $D_0/A_E$ ) pulp, on the other hand, nearly doubled this incremental brightness gain across the  $D_1$  stage. This result was not unexpected because the ( $D/A_E$ ) pulps contained more extractable lignin, which consumed some of the applied  $ClO_2$ . The brightness of ( $D_0/A_E$ ) $E$  $D_1$  pulps were generally 5 to 10 points lower than  $D_0E$  $D_1$  pulps.

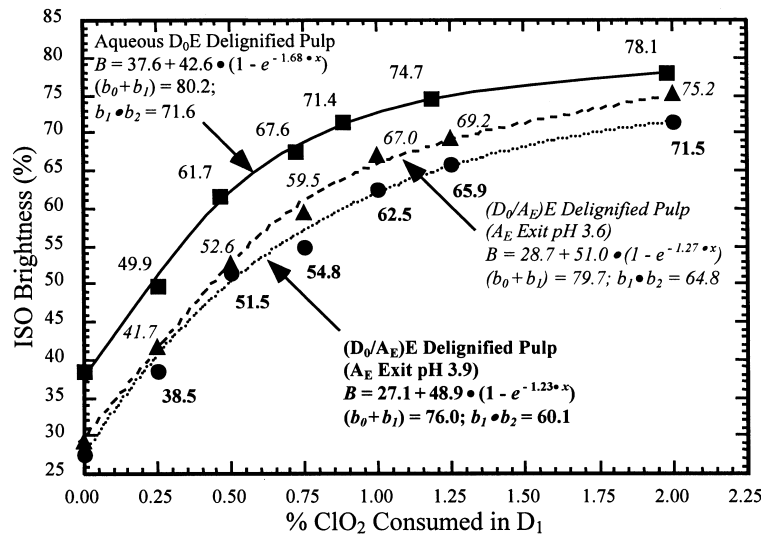
Several aqueous  $D_1$  runs, at various applied  $ClO_2$  levels, were performed on ( $D_0/A_E$ )E and aqueous  $D_0E$  pulps to obtain brightness response curves (Figure 1). Both ( $D_0/A_E$ )E pulps afforded lower post- $D_1$  brightness levels than aqueous  $D_0E$  pulps at given amounts of  $ClO_2$  consumed. The ( $D_0/A_E$ )E pulp at a 3.6  $A_E$  exit pH generally required ~65% more  $ClO_2$  to



**Table 6.** Brightness Development of Ethanol-Based (D<sub>0</sub>/A<sub>E</sub>)- and Aqueous D<sub>0</sub>E-Treated Pulps with 1.25% ClO<sub>2</sub> in D<sub>1</sub> Stage

Bleaching sequence prior to D <sub>1</sub> stage <sup>†</sup>	A <sub>E</sub> stage exit pH	ISO brightness (%)	
		Pre-D <sub>1</sub>	Post-D <sub>1</sub>
Aqueous D <sub>0</sub> E	–	38.5	74.1
(D <sub>0</sub> /A <sub>E</sub> )	3.6	22.9	45.5
(D <sub>0</sub> /A <sub>E</sub> )	3.9	21.7	45.1
(D <sub>0</sub> /A <sub>E</sub> )E	3.6	29.2	69.2
(D <sub>0</sub> /A <sub>E</sub> )E	3.9	27.6	65.9

<sup>†</sup>All E stages performed with 100% aqueous medium; 2.5-hr. A<sub>E</sub> stage.



**Figure 1.** D<sub>1</sub>-stage brightness response curves for (D<sub>0</sub>/A<sub>E</sub>)E- and D<sub>0</sub>E-treated pulps (Table 6). Response curves are based on Eq. 1. An aqueous medium was used in all E and D<sub>1</sub> stages.

achieve a given D<sub>1</sub> brightness level than a D<sub>0</sub>E pulp that had a similar amount of residual lignin.

The results in Figure 1 were fitted to a simple brightening model that has been used to characterize pulp bleachability:<sup>19</sup>

$$B = b_0 + b_1 \cdot (1 - e^{-b_2 x}) \quad (1)$$



where  $B$  is the predicted pulp brightness,  $x$  is the consumed amount of  $\text{ClO}_2$ ,  $b_0$  is the entering pulp brightness, and  $b_1$  is the brightness gain across the  $D_1$ . The sum  $(b_0 + b_1)$  represents the asymptotic brightness limit of the  $D_1$  stage, and the last parameter,  $b_2$ , denotes the relative rate at which this asymptotic limit is approached.<sup>19</sup>

Equation 1 modeled the brightening response data well ( $R^2 > 0.99$ ) and quantitatively indicated the lower bleachability of  $(D_0/A_E)E$  pulps (Figure 1). The model predicts that  $(D_0/A_E)E$  and  $D_0E$  pulps, which have similar residual lignin levels, will approach a common  $D_1$  brightness ceiling of  $\sim 80$  ISO, whereas the  $(D_0/A_E)E$  pulp with the higher residual lignin will have a lower asymptotic limit ( $\sim 76$  ISO). The  $D_1$  initial response factor,  $b_1 \cdot b_2$ , represents the initial slope of the brightness response curve (Eq. 1). A high  $b_1 \cdot b_2$  value indicates a quick brightening response to a low level of consumed  $\text{ClO}_2$ .<sup>19</sup> The lower  $b_1 \cdot b_2$  values for the  $(D_0/A_E)E$  pulps clearly indicate the slower brightening response to  $\text{ClO}_2$ .

### Possible Factors Affecting $(D_0/A_E)$ Bleachability

The results of the  $D_1$  bleachability study clearly established that  $(D_0/A_E)$  and  $(D_0/A_E)E$  pulps are more difficult to brighten than aqueous-based  $D_0E$  pulps. Part of the bleachability difference between the ethanol-based partial sequence and the conventional aqueous sequence is related to the  $A_E$  stage. The  $A_E$  stage is not as proficient or as selective at removing dissolvable lignin as an aqueous  $E$  stage; this lower delignification efficiency is presumably related to physico-chemical limiting factors.<sup>7,9,11</sup> In addition, the  $A_E$  stage increases the amount of chromophoric groups in the pulp, as is indicated by the higher value of  $k_{457}$  (Table 6). These  $k_{457}$  values after the  $A_E$  are close to the original  $k_{457}$  value of the unbleached pulp, although the  $(D_0/A_E)$  pulps have less residual lignin. These new chromophoric groups decrease pulp brightness, increase  $\text{ClO}_2$  consumption, and furthermore, may be more resistant to  $\text{ClO}_2$  attack. At this time, it is unknown what types of chromophoric groups are produced during the  $A_E$  stage.

Another factor possibly influencing  $D_1$  bleachability of  $(D_0/A_E)$  pulps is the previous  $D_0$  stage. We have shown in an earlier study<sup>20</sup> that an ethanol-based  $D_0$  stage yields an oxidized residual lignin that has more quinone structures than an aqueous  $D_0$  stage. These structures could subsequently polymerize<sup>12,13,21</sup> in the  $A_E$  stage forming new structures, which result in a more difficult lignin to alkali extract and/or bleach in a  $D_1$  stage.



**Bleachability of Ethanol- Versus Aqueous-based D<sub>0</sub> Delignified Pulps**

The results from the previous section illustrated that the A<sub>E</sub> stage is ineffective at lignin removal and negatively impacts future bleachability. However, looking back at the data from Table 5 on the various delignification sequences, we see that an ethanol-based D<sub>0</sub> stage provides a pulp that has 2 units higher brightness and slightly lower  $k_{457}$  than its aqueous counterpart. Apparently, the oxidized lignin in the ethanol-based D<sub>0</sub> pulps is less colored than the oxidized lignin in aqueous D<sub>0</sub> pulps.

Aqueous E stages performed on these pulps yielded some interesting results (Table 7). After extraction, the ethanol D<sub>0</sub> pulp had approximately the same kappa number and total residual lignin level as the aqueous D<sub>0</sub> pulp. However, the aqueous D<sub>0</sub> pulp had a higher brightness after extraction than the ethanol D<sub>0</sub> pulp. In addition, the brightness of the aqueous D<sub>0</sub> pulp increased 5 points during caustic extraction as compared to the brightness of the ethanol D<sub>0</sub> pulp, which increased by 1 point. There was little change in the  $k_{457}$  for the ethanol D<sub>0</sub> pulp after an aqueous E stage, whereas the  $k_{457}$  for the aqueous D<sub>0</sub> pulp decreased by ~25%.

The D<sub>0</sub>E delignified pulps were subjected to aqueous D<sub>1</sub> stages to observe how the D<sub>0</sub> treatment impacts D<sub>1</sub> brightness. The D<sub>1</sub> brightness responses for these pulps, at various applied ClO<sub>2</sub> levels, are given in Figure 2. The pulps treated with an aqueous D<sub>0</sub> stage appeared easier to bleach with the D<sub>1</sub> stage, at a given ClO<sub>2</sub> charge, than pulps treated with an ethanol D<sub>0</sub>, even though the two D<sub>0</sub>E delignified pulps have approximately the same amount of residual lignin entering into the D<sub>1</sub> stage. Ethanol D<sub>0</sub> pulps

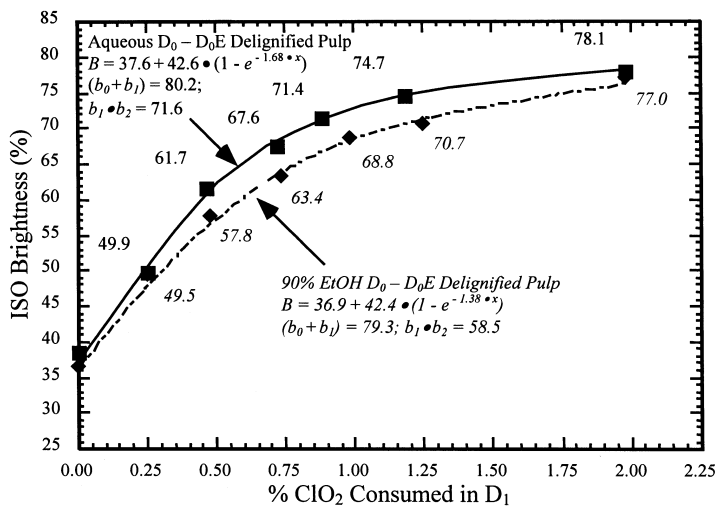
**Table 7.** Effects of D<sub>0</sub> Bleaching Medium on Subsequent Aqueous E-Stage Brightness, Residual Lignin Removal, and Chromophore Reduction (i.e.,  $k_{457}$ )

Type of pulp	ISO brightness (%)	Kappa number	Residual lignin (%)	Light absorption coeff. $k_{457}$ (m <sup>2</sup> /kg)
Unbleached pulp	19.7	30.1	4.61	15.7
Aqueous D <sub>0</sub> stage				
Pre-caustic extraction	32.4	16.2	2.98	4.8
Post-caustic extraction	37.9	7.3	1.37	3.6
Ethanol-based D <sub>0</sub> stage				
Pre-caustic extraction	34.9	13.6	2.99	3.8
Post-caustic extraction	35.7	7.7	1.41	3.7

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**Figure 2.** D<sub>1</sub>-stage brightness response curves for D<sub>0</sub>E-delignified pulps where either a 90% ethanol or an aqueous medium used in D<sub>0</sub> stage (Table 7). Response curves are based on Eq. 1. An aqueous medium was used in all E and D<sub>1</sub> stages.

consumed ~20% more ClO<sub>2</sub> to reach a given D<sub>1</sub> brightness level than the aqueous counterpart. Only trace ClO<sub>2</sub> residuals were detected in the D<sub>1</sub> effluents for ethanol D<sub>0</sub> pulps; aqueous D<sub>0</sub> pulps, on the other hand, were observed to have residuals up to 10% of applied ClO<sub>2</sub> charge in the D<sub>1</sub> effluents.

The data in Figure 2 were fitted to the simple brightening model (Eq. 1) to better characterized D<sub>1</sub> bleachability. Both D<sub>0</sub>E pulps are predicted to reach a common D<sub>1</sub> brightness ceiling of ~80% ISO. The D<sub>0</sub> bleaching medium did not appear to effect the maximum brightness gain (*b*<sub>1</sub>) in the D<sub>1</sub> stage. However, the relative rate at which this brightness gain is approached is slower for the D<sub>0</sub> stage pulp bleached in an ethanol medium relative to an aqueous medium. As expected, the ethanol D<sub>0</sub> pulp had a lower *b*<sub>1</sub>·*b*<sub>2</sub> value, suggesting that the remaining lignin is more difficult to brighten in a D<sub>1</sub> stage.

### Possible Factors Affecting D<sub>0</sub>E Bleachability

In addition to affecting the post-D<sub>0</sub> kappa number and brightness, the D<sub>0</sub> solvent had a significant influence on the subsequent E and D<sub>1</sub> stage brightening response of the pulp. Our previous study, which examined D<sub>0</sub>

stage delignification of ethanol- and aqueous-based systems, showed that residual lignin of ethanol  $D_0$  pulps has more quinone structures than an aqueous-based  $D_0$  stage.<sup>20</sup> The slow brightening response of ethanol  $D_0$  pulps in the  $D_1$  stage may be the result of additional quinone-type structures in the residual lignin. Brage *et al.*<sup>13</sup> have indicated that  $ClO_2$  does not react with quinones to any appreciable extent; however, the authors point out that intermediate  $ClO_2^-$ , arising from other  $ClO_2$  reactions, can react with quinones to afford oxidation products. These quinone structures are slowly eliminated during the  $D_1$  when a sufficient amount of  $ClO_2^-$  has accumulated.

## CONCLUSIONS

An ethanol-based ( $D_0/A_E$ ) sequence using the  $D_0$  effluent as the  $A_E$  medium generally showed improved delignification to that observed in the  $D_0A_E$  sequence. This improved delignification appeared to be related to the low concentrations of residual  $ClO_2^-$  from the  $D_0$  effluent. The  $A_E$  stage is less efficient and selective at extracting dissolvable lignin than an aqueous E stage. Furthermore, the  $A_E$  stage generated additional chromophoric groups that persisted even after an aqueous E stage. Alkali extracted ( $D_0/A_E$ ) pulps were more difficult to brighten in a  $D_1$  stage than aqueous DE pulps. This lower  $D_1$  bleachability of ( $D_0/A_E$ ) delignified pulps is presumably related to changes in the residual lignin during both  $D_0$  and  $A_E$  stages.

Ethanol-based  $D_0$  stages yielded pulps with higher brightness levels than the aqueous controls. However, aqueous  $D_0$  pulps were slightly brighter than the ethanol  $D_0$  pulps after an aqueous caustic extraction stage. The extracted ethanol  $D_0$  pulps were more difficult to brighten in a  $D_1$  stage than the corresponding aqueous  $D_0E$  pulps. Presumably, the alterations in the residual lignin structure caused by an ethanol  $ClO_2$  oxidation<sup>7,20</sup> adversely affects  $D_1$  bleachability.

## EXPERIMENTAL

### Pulp Bleaching

A conventional kraft pulp (southern pine) was obtained from a mill and used throughout this study. Additional details about the pulping conditions are provided in previous reports.<sup>7,8</sup> The pulp had a kappa number of 30.1 and a viscosity of 25.1 mPas. The  $D_0$  stage was performed either with a 90% (v/v) ethanol or a 100% aqueous medium at the following



conditions: 2.52%  $\text{ClO}_2$  on o.d. pulp (0.22 kappa factor), 3% consistency, initial pH 4.2–4.6 prior to  $\text{ClO}_2$  addition, 70°C, and 15-min. reaction time. The  $D_0$  filtrate contained no significant residual  $\text{ClO}_2$  and had an exit pH of 2.2 to 2.6.

Acid ethanol extractions ( $A_E$  stages) were performed on  $D_0$  pulps bleached in a 90% ethanol medium. The extraction medium was either a fresh 90% ethanol solution or the previous  $D_0$  effluent (i.e.,  $(D_0/A_E)$  sequence). Sodium hydroxide or sodium acetate was added such that the  $A_E$  exit pH was  $\sim 3.4$  to 4.2. All  $A_E$  stages were done at 3% consistency. Small- and large-scale  $A_E$  stages were performed in 300-mL and 2-L stirred Parr<sup>®</sup> bomb reactors, respectively, equipped with heating mantles and temperature controllers. Pulps were extracted for 2.5 h (unless otherwise noted) at 130°C, cooled to  $\sim 65^\circ\text{C}$ , and drained of extraction effluent to  $\sim 25\%$  consistency. Afterwards, the pulp was washed first with 90% ethanol and later with copious amounts of deionized (DI) water. Technical grade  $\text{NaClO}_2$  ( $\sim 80\%$  purity) was used in selected  $A_E$ -stage experiments.<sup>7</sup>

All E stages were performed with a 100% aqueous medium at the following conditions: 3.64% NaOH on o.d. pulp (0.55 caustic multiple), 10% consistency, 60°C, and 60-min. reaction time. All  $D_1$  stages were performed with 100% aqueous medium under the following conditions: 10% consistency, 70°C, and 3-h reaction time. An amount of NaOH was added to the pulp, after the  $\text{ClO}_2$  addition, such that the pulp slurry pH dropped to  $\sim 4.3$  pH after 15 min of reaction. Generally, the  $D_1$  effluent had an ending pH between 3.6 and 4.5. Both E and  $D_1$  stages were conducted in Kapak<sup>®</sup>/Scotchpack sealable pouches. Residual  $\text{ClO}_2$  in the  $D_1$  effluent was determined idometrically.<sup>7</sup>

### Analytical Measurements

Kappa numbers were determined by micro-kappa number measurements (TAPPI Useful Method UM-246). ISO brightness (TAPPI Standard T-525 om-92) and dry zero-span breaking length (TAPPI Standard T-231 cm-85) measurements were made on selected treated pulps. Wet zero-span measurements were done by the above dry zero-span method except that the paper strips were briefly immersed in ultra-pure DI water and blotted dry prior to testing. Unused paper strips from the zero-span analyses were utilized for pulp viscosity measurements (TAPPI Standard T-230 om-89). Residual lignin was determined by the UV spectroscopic method described by Mallett<sup>22</sup> using a wavelength of 295 nm and lignin absorptivity value of 19.6 L/(g-cm).<sup>7,20</sup>



Light absorption coefficients at 457 nm ( $k_{457}$ ) were measured on selected handsheets using a Technibrite Micro TB-1C brightness meter equipped with an opacity function. The basic guidelines of the measurement are given in TAPPI Standard T-425 om-91 and by Teder and Tormund.<sup>23</sup> All  $k_{457}$  values reported had corresponding light-scattering coefficients ( $s_{457}$ ) of 24.6 to 28.0 m<sup>2</sup>/kg.<sup>7</sup>

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